Original Article

Predicting stomatal responses to the environment from the optimization of photosynthetic gain and hydraulic cost

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ABSTRACT

Stomatal regulation presumably evolved to optimize CO₂ for H₂O exchange in response to changing conditions. If the optimization criterion can be readily measured or calculated, then stomatal responses can be efficiently modelled without recourse to empirical models or underlying mechanism. Previous efforts have been challenged by the lack of a transparent index for the cost of losing water. Yet it is accepted that stomata control water loss to avoid excessive loss of hydraulic conductance from cavitation and soil drying. Proximity to hydraulic failure and desiccation can represent the cost of water loss. If at any given instant, the stomatal aperture adjusts to maximize the instantaneous difference between photosynthetic gain and hydraulic cost, then a model can predict the trajectory of stomatal responses to changes in environment across time. Results of this optimization model are consistent with the widely used Ball–Berry–Leuning empirical model (r² > 0.99) across a wide range of vapour pressure deficits and ambient CO₂ concentrations for wet soil. The advantage of the optimization approach is the absence of empirical coefficients, applicability to dry as well as wet soil and prediction of plant hydraulic status along with gas exchange.

Key-words: Ball–Berry–Leuning model; Cowan–Farquhar optimization; hydraulic limitations; photosynthetic optimization; plant drought responses; plant gas exchange; stomatal modelling; stomatal regulation; xylem cavitation.

INTRODUCTION

Land plants face a fundamental carbon-for-water trade-off. They must open their stomata for photosynthetic gain, but doing so promotes water loss. Plant responses to environment represent a balancing act that presumably optimizes this trade-off in some manner (Cowan & Farquhar 1977; Katul et al. 2010; Manzoni et al. 2011; Medlyn et al. 2011; Bonan et al. 2014; Prentice et al. 2014). When air and soil are dry, photosynthesis is sacrificed in favour of reduced water loss (Schulze & Hall 1982). When ambient CO₂ is scarce, greater water loss is tolerated in favour of photosynthesis (Morison 1987). The trade-off has seemingly resulted in tight coordination between capacity to supply and transpire water (hydraulic conductance, k, and diffusive conductance to water vapour, Gw) and the maximum capacity for photosynthesis (carboxylation rate, Vmax, and electron transport rate, Jmax; Brodribb et al. 2002). If the fulcrum on which this trade-off balances could be identified, it would greatly simplify the difficult problem of predicting how plant gas exchange responds to environmental cues (Prentice et al. 2014). In this paper, we describe such a balancing point, explain how it can be readily quantified from measurable plant traits and processes, and evaluate the resulting patterns in stomatal regulation of gas exchange and xylem pressure.

The utility of a stomatal optimization framework has long been recognized, but uncertainty in the optimization criteria and its relation to true fitness costs and benefits has limited its potential for understanding and modelling stomatal behaviour, particularly in response to drying soil. A long-standing theory (Cowan & Farquhar 1977) assumes stomatal regulation maximizes cumulative photosynthesis (A) for a fixed amount of water transpired (cumulative E) over a time period. This is a ‘constrained-optimization’ problem (total E is constrained) whose solution specifies a constant Lagrangian multiplier, λ', which equals a constant δE/δA. Stomata are assumed to maintain δE/δA = λ' at every instant throughout the time period, and this behaviour can be modelled (Cowan & Farquhar 1977; Cowan 1982; Makala et al. 1996; Medlyn et al. 2011; Manzoni et al. 2013). But a persistent problem is in putting an a priori number on λ'. Which of the infinite values for δE/δA is the right one? The δE/δA is assumed to represent the ‘unit marginal cost’ (δcost/δgain) where the cost of stomatal opening is equated with E and A is the gain (Cowan 1982; p. 591). But it has been challenging to specify the optimal marginal cost, and how it might vary with species, environment and time (Givnish 1986; Manzoni et al. 2011; Manzoni et al. 2013; Buckley et al. 2016).

A related issue is whether the optimization problem is properly framed (Woll et al. 2016). Instead of maximizing photosynthesis for an arbitrarily fixed amount of water loss over some period of time, is it not more to the point that plants would maintain the greatest carbon gain relative to the actual cost of water loss at all times, regardless of the amount of water used or time period involved? Such plants will use more water when
it is cheap and there is opportunity for more photosynthetic gain, and they will use less water when its cost rises or there is less photosynthetic opportunity. In this ‘profit maximization’ optimization, there is no arbitrary constraint on the amount of water the plant can use over time, and there is no constant Lagrangian multiplier involved in its solution (no $\lambda$). The equation is: \[ \text{profit} = \text{gain} - \text{cost}. \] Maximum profit is found by setting the derivative of this equation to zero, at which point \[ \text{cost} / \text{gain} = 1. \] In profit maximization, the unit marginal cost should always equal 1. But to implement this scheme, the cost of water use must be specified.

After the leaf scale concept of coupled carbon and water economy arose we have learned how xylem cavitation limits the transpiration stream (Tyree & Sperry 1988; Sperry et al. 1998; Sperry & Love 2015). As the physiological importance of cavitation became accepted, a second perspective on stomatal regulation emerged, which is that stomata act to maximize photosynthesis under the constraint of avoiding excessive xylem cavitation (Feild & Holbrook 1989; Sparks & Black 1999; Tombesi et al. 2015; Novick et al. 2016). It is possible to model stomatal behaviour in response to water stress solely on the principle that stomata close in proportion to the threat of cavitation on canopy water supply (Sperry & Love 2015; Sperry et al. 2016). While this hydraulic approach may prove practical in many applications, it ignores the role of stomata in regulating and responding to photosynthesis, and it does not emerge explicitly from the carbon-for-water tradeoff. However, it does identify the loss of conductivity to cavitation as an important fitness cost of moving water. Mortality is the ultimate fitness cost, and it exhibits a strong linkage to vascular dysfunction (Kukowski et al. 2013; McDowell et al. 2013; Anderegg et al. 2015; Anderegg et al. 2016).

Perhaps, the hydraulic models are providing a proxy for the cost of water loss, thus allowing the implementation of the profit maximization theory. Hydraulics provide a ‘cost’ function for stomatal opening, and the corresponding photosynthetic ‘gain’ function can be obtained from trait- and process-based models of photosynthesis. The stomatal regulation that maximizes the profit (where \( \text{cost} / \text{gain} = 1 \)) can be modelled on this basis. In this paper, we develop this perspective and explore its potential for improving our understanding and ability to model stomatal responses to environmental forcing. Its predictions are compared to those of a purely hydraulic model for stomatal conductance (Sperry & Love 2015; Sperry et al. 2016) and to a widely used empirical model (Ball, Berry, Leuning [BBL]; Leuning 1995). The contrast in stomatal behaviour between profit maximization versus the \( \partial \text{E} / \partial \text{A} = \lambda \) constrained optimization is discussed.

Stomatal response modelling does need improvement. We can model leaf energy balance, photosynthesis, hydraulic conductance and transpiration reasonably well under any environmental situation if the diffusive conductance of the leaf (\( G_w \)) is known (Collatz et al. 1991; Collatz et al. 1992). In lieu of a trait and process-based predictive model for stomatal control of \( G_w \) models, we have relied on empirical relationships. Conventional formulations employed by land-surface models assume an empirical model for the \( G_w \) response to atmospheric vapour pressure deficit (\( D \)), photosynthetic rate (\( A \)) and ambient CO₂ concentration (\( C_a \)) under wet soil conditions (e.g. the BBL model; Leuning 1995). The wet soil model is scaled with a second empirical model to yield the \( G_w \) response to soil water potential (\( P_s \); Powell et al. 2013). Besides the unsatisfying need to rely on empirical coefficients of unknown physiological meaning, these coefficients must be either robust to widely different plant and soil types or else known for relevant functional types. The stomatal response to drying soil is especially challenging (Williams et al. 1996; Darmour et al. 2010; Manzoni et al. 2011; Manzoni et al. 2013; Powell et al. 2013). Hence, the search continues for a better way to model stomatal responses that is grounded in relevant process and measurable traits.

THE MODEL

The hydraulic cost function

The hydraulic cost function is based on a ‘supply function’ which describes the theoretical steady-state relation between \( E \) and canopy xylem pressure (\( P_x \)) at a given root zone soil water potential, \( P_s \) (Fig. 1a blue \( E \) curve for \( P_s = 0 \); Fig. 1c blue curve for \( P_s = -1 \text{ MPa} \)). Supply functions are calculated from soil and xylem vulnerability curves that describe how hydraulic conductance (\( k \)) of a soil or plant component declines from its maximum (\( k_{\text{max}} \)) in response to negative water pressure (\( P \)):

\[
k = k_{\text{max}} f(P).
\]

(1a)

For the plant, a two-parameter Weibull function for \( f(P) \) describes a wide range of vulnerability curves (Neufeld et al. 1992):

\[
f(P) = e^{-\left((P/P_f)^{b}\right)},
\]

(1b)

analogous to the van Genuchten function used for in soil (van Genuchten 1980). The Weibull ‘\( b \)’ parameter is \( P \) at \( k/k_{\text{max}} = 0.37 \), and \( e \) controls whether the curve is a threshold sigmoidal form (\( c > 1 \)) or non-threshold ‘exponential’ curve (\( c < 1 \)). Transpiration (\( E \)) induces a pressure drop (upstream \( P \) – downstream \( P = P_{\text{up}} - P_{\text{down}} \)) across each soil and xylem element. At steady-state, \( E \) is the integral of each element’s vulnerability curve from \( P_{\text{up}} \) to \( P_{\text{down}} \) (Sperry & Love 2015):

\[
E = \int_{P_{\text{up}}}^{P_{\text{down}}} k_{\text{max}} f(P) \, dP.
\]

(2)

By integrating across all vulnerability curves in the soil–plant system, the relation between \( E \) and a given total \( P_s - P_c \) pressure drop can be found. This ‘supply function’ starts at \( E = 0 \) at \( P_c = P_s \), and rises to \( E = E_{\text{crit}} \) at \( P_c = P_{\text{crit}} \) (Fig. 1a, blue \( E \) curve, expressed per leaf area). It is a curve of increasing damage and risk. The curve is steepest and nearly linear at first when pressures are modest and cavitation is minimal. It begins to flatten as cavitation reduces hydraulic conductance and more pressure drop is required to move water. The instantaneous slope of the supply function at \( P_c \) is proportional to the hydraulic conductance in the canopy (\( k_c \propto \partial E / \partial P_c \); Sperry et al. 2016). The \( k_c \) declines from a maximum at \( E = 0 \) (\( k_{\text{max}} \)) to near 0 (\( k_{\text{crit}} \)) at \( E = E_{\text{crit}} \) (Fig. 1a, end of blue \( E \) curve). The \( f(P) \) functions (Eqn 1b and soil van Genuchten curves) do
not go to mathematical zero, so $k_{crit}$ represents a ‘physiological zero’ set to 0.05% of $k_{max}$ by this point increases in $E$ (beyond $E_{crit}$) have become undetectable (Fig. 1a). At $E_{crit}$ the supply system has reached its limit: no greater steady-state transpiration rate is possible without driving canopy conductance to zero and desiccating the canopy.

In the hydraulic model of Sperry and Love (Sperry & Love 2015; Sperry et al. 2016), stomata are assumed to regulate the $\Delta P = P_{t} - P_{c}$ pressure drop based on the fractional drop in canopy hydraulic conductance from its maximum $(k_{c}/k_{max})$: 

$$\Delta P = \Delta P^{c} \frac{k_{c}}{k_{max}}.$$  

where $\Delta P^{c}$ is the unregulated pressure drop. This regulated $\Delta P$ yields the regulated values for $E$ and $P_{c}$, and also the diffusive leaf conductance to water vapour ($G_{w} = E / D_{L}$; $D_{L}$ is leaf-to-air vapour pressure deficit; $G_{w}$ includes stomatal and boundary layer components). As $\Delta P^{c}$ increases, $\Delta P$ rises to a maximum and then falls as $k_{c}/k_{max}$ approaches zero. The hydraulic model assumes $\Delta P$ saturates at the maximum, consistent with the tendency for $E$ and $P_{c}$ to saturate as $D_{L}$ increases.

Here, we move beyond the purely hydraulic approach and use the supply function to derive a transpirational ‘cost function’ $(\theta(P_{c}))$ that reflects the increasing damage from cavitation and greater difficulty of moving the transpiration stream:

$$\theta(P_{c}) = \frac{k_{max} - k_{c}(P_{c})}{k_{max} - k_{crit}},$$

where $k_{c}$ is evaluated at $P_{c}$. The $\theta$ is the fractional loss of canopy (downstream) hydraulic conductance, which rises to $\theta=1$ at hydraulic failure. As shown in Fig. 1b (blue $\theta$ curve, see also Fig. 1d for $P_{c} = -1$ MPa), $\theta$ rises relatively slowly from zero at $P_{c} = P_{crit}$ ($k_{c} = k_{crit}$) because limited cavitation at modest $P_{c}$ means water is cheap. However, as $P_{c}$ becomes more negative and more cavitation is induced, $\theta$ accelerates before gradually approaching 1 at $P_{c} = P_{crit}$ ($k_{c} = k_{crit}$) where the plant pays the ultimate cost of canopy desiccation. The normalization removes units and relates cost to hydraulically defined end-points corresponding to a particular species (e.g. $P_{crit}$) and a specific point in time (root zone $P_{r}$).

The model of Sperry et al. 2016 was used to compute the supply- and cost functions (Fig. 1, blue curves in (a)–(d)). For all simulations in this paper, their model was run in

![Figure 1. Stomatal response model based on the optimization of photosynthetic gains and hydraulic costs. (a) The blue supply function is the steady state relationship between transpiration ($E$) and canopy xylem pressure ($P_{c}$) that is calculated from the continuum vulnerability curves and soil water potential ($P_{s}$). The supply function terminates at $E_{crit}$ (and the associated $P_{crit}$) beyond which hydraulic failure and canopy desiccation occurs. Under certain conditions (high $P_{c}$ and low $D$) maximal diffusive conductance ($G_{max}$) can limit $E$ and $P_{c}$. The $E$ curve is used to calculate consecutively: 1) the leaf temperature ($T_{c}$), 2) leaf-to-air vapour pressure deficit ($D_{L}$) and 3) diffusive conductance of leaf to water vapour ($G_{w}$) and CO$_{2}$ ($G_{w}$, not shown). The $G_{c}$ is then used to calculate 4) internal leaf CO$_{2}$ concentration ($C$) and 5) the gross assimilation rate ($A$) from a modelled $A-C_{c}$ curve. These six curves represent the continuum of possible steady states at a given instant in time. The plant can ‘choose’ any state by adjusting its $G_{w}$ via stomatal control. (b) The hydraulic cost function (blue $\theta$ curve) is the fractional loss of downstream hydraulic conductance that is calculated from the $E(P_{c})$ supply function. The $\theta$ rises from zero at $P_{c} = P_{crit}$ to 1 at $P_{c} = P_{crit}$. The carbon gain function ($\beta$) is the fractional increase in $A$ from 0 at $P_{c} = P_{crit}$ to 1 at its instantaneous maximum as calculated from the $A(P_{c})$ curve in (a). Stomata are assumed to maintain the plant at the optimum where $\beta-\theta$ (black curve) is maximized ($\text{Profit}_{max}$); $\text{Profit}_{max}$ coincides with $\partial \beta/\partial P_{c} = \partial \theta/\partial P_{c}$ (tangents on $\beta$ and $\theta$ curves). The optimum specifies $P_{c}$ and hence the six parameters in (a). (c) The six curves in (a) corresponding to $P_{c} = -1$ MPa (versus $P_{c} = 0$ in (a)). (d) The shift in cost ($\theta$) and gain ($\beta$) functions associated with $P_{c} = -1$. The new $\beta-\theta$ optimum predicts the shift in $P_{c}$ and hence the change in the six parameters in (c).]
unsegmented mode (all xylem components assigned the same Weibull \( f(P) \) function), with the xylem being limiting (rhizosphere average resistance of 5%). The model runs in reversible and irreversible cavitation modes, but for the present purpose reversibility was moot because all simulations were run from low to high water stress. The Sperry et al. model was revised to express conductances on a leaf area basis to allow energy balance and photosynthesis calculations (‘big-leaf’ canopy composed of identical leaves). The revised model is a Visual Basic for Applications macro in Microsoft Excel (code available from the senior author). Hydraulic parameters underlying the supply function are listed in Table 1.

### Table 1. Main inputs and outputs of the hydraulic cost and photosynthetic gain optimization model

<table>
<thead>
<tr>
<th>Abbreviation</th>
<th>Variable or parameter description</th>
<th>Default (test values)a</th>
<th>Units</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Inputs</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>(a) Environmental drivers</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>( C_a )</td>
<td>Atmospheric CO(_2) concentration</td>
<td>40 (15–65)</td>
<td>Pa</td>
</tr>
<tr>
<td>( D )</td>
<td>Atmospheric water pressure deficit</td>
<td>1 (0.10–4.26)</td>
<td>kPa</td>
</tr>
<tr>
<td>( O_a )</td>
<td>Atmospheric O(_2) concentration</td>
<td>21 000</td>
<td>Pa</td>
</tr>
<tr>
<td>( P_{atm} )</td>
<td>Atmospheric air pressure</td>
<td>101.3</td>
<td>kPa</td>
</tr>
<tr>
<td>( P_s )</td>
<td>Soil water potential</td>
<td>0 (to –7)</td>
<td>MPa</td>
</tr>
<tr>
<td>( Q )</td>
<td>PAR photon flux density</td>
<td>2000 (0–2000)</td>
<td>( \mu )mol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( T_A )</td>
<td>Air temperature</td>
<td>25 (30(^{b}), 10–40(^{c}))</td>
<td>°C</td>
</tr>
<tr>
<td>( u )</td>
<td>Wind speed</td>
<td>2</td>
<td>m s(^{-1})</td>
</tr>
<tr>
<td>(b) Hydraulic cost and photosynthetic gain parameters</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>( c )</td>
<td>Curvature of the light response curve</td>
<td>0.9</td>
<td></td>
</tr>
<tr>
<td>( c' )</td>
<td>Curvature factor for ( J_e ) versus ( J_l ) limited photosynthesis</td>
<td>0.98</td>
<td></td>
</tr>
<tr>
<td>( d )</td>
<td>Leaf width ( \times 0.72 )</td>
<td>0.0072</td>
<td>m</td>
</tr>
<tr>
<td>( G_{max} )</td>
<td>Maximum diffusive conductance to water vapour</td>
<td>Set by ( V_{max25} )</td>
<td>mmol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( J_{max25} )</td>
<td>Maximum electron transport rate at 25 °C</td>
<td>1.67 ( V_{max25} )</td>
<td>( \mu )mol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( K_e )</td>
<td>Michaelis–Menten constant for carboxylation</td>
<td>41 at 25 °C</td>
<td>Pa</td>
</tr>
<tr>
<td>( K_c )</td>
<td>Michaelis–Menten constant for oxygenation</td>
<td>28 202 at 25 °C</td>
<td>Pa</td>
</tr>
<tr>
<td>( k_{max} )</td>
<td>Maximum soil-canopy hydraulic conductance per leaf area</td>
<td>Set by ( V_{max25} )</td>
<td>mmol s(^{-1}) m(^{-2}) MPa(^{-1})</td>
</tr>
<tr>
<td>( R_{abs} )</td>
<td>Absorbed long- and short-wave radiation</td>
<td>740</td>
<td>W m(^{-2})</td>
</tr>
<tr>
<td>( V_C )</td>
<td>Two parameter ([h, c] ) Weibull vulnerability curve</td>
<td>([2,3] ) ([1,3] ), ([3,3] ), ([2,1] ) (d)</td>
<td></td>
</tr>
<tr>
<td>( V_{max25} )</td>
<td>Maximum carboxylation rate at 25 °C</td>
<td>100 (25–150)</td>
<td>( \mu )mol s(^{-1}) mol(^{-1})</td>
</tr>
<tr>
<td>( \Gamma^* )</td>
<td>CO(_2) compensation point</td>
<td>4.36 at 25 °C</td>
<td>Pa</td>
</tr>
<tr>
<td>( \epsilon )</td>
<td>Emissivity</td>
<td>0.97</td>
<td></td>
</tr>
<tr>
<td><strong>Outputs</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>( A )</td>
<td>Gross assimilation rate</td>
<td></td>
<td>( \mu )mol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( A_{max} )</td>
<td>Instantaneous maximum gross assimilation rate</td>
<td></td>
<td>( \mu )mol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( C_l )</td>
<td>Internal leaf CO(_2) concentration</td>
<td></td>
<td>Pa</td>
</tr>
<tr>
<td>( D_l )</td>
<td>Leaf to air water pressure deficit</td>
<td></td>
<td>kPa</td>
</tr>
<tr>
<td>( E )</td>
<td>Canopy transpiration rate</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( E_{crit} )</td>
<td>Transpiration rate limit (values above desiccate the canopy)</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( G_{C_l} )</td>
<td>CO(_2) diffusive conductance of leaf</td>
<td></td>
<td>( \mu )mol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( G_e )</td>
<td>( H_2O ) vapour diffusive conductance of leaf</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2})</td>
</tr>
<tr>
<td>( k )</td>
<td>Hydraulic conductance (per leaf-area)</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2}) MPa(^{-1})</td>
</tr>
<tr>
<td>( k_c )</td>
<td>Canopy hydraulic conductance (per leaf area)</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2}) MPa(^{-1})</td>
</tr>
<tr>
<td>( k_{crit} )</td>
<td>Canopy hydraulic conductance when ( E_{crit} ) is reached</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2}) MPa(^{-1})</td>
</tr>
<tr>
<td>( k_{max} )</td>
<td>Maximum canopy hydraulic conductance</td>
<td></td>
<td>mmol s(^{-1}) m(^{-2}) MPa(^{-1})</td>
</tr>
<tr>
<td>( Profit_{max} )</td>
<td>Maximum profit ([\beta-\theta_{max}] ), indicating optimal stomatal conductance for current environmental conditions</td>
<td></td>
<td></td>
</tr>
<tr>
<td>( P_C )</td>
<td>Canopy xylem pressure</td>
<td></td>
<td>MPa</td>
</tr>
<tr>
<td>( P_{crit} )</td>
<td>Canopy xylem pressure at ( E_{crit} )</td>
<td></td>
<td>MPa</td>
</tr>
<tr>
<td>( \Delta P )</td>
<td>Regulated pressure drop between soil and canopy</td>
<td></td>
<td>MPa</td>
</tr>
<tr>
<td>( \Delta P' )</td>
<td>Unregulated pressure drop between soil and canopy</td>
<td></td>
<td>MPa</td>
</tr>
<tr>
<td>( T_L )</td>
<td>Leaf temperature</td>
<td></td>
<td>°C</td>
</tr>
<tr>
<td>( \beta )</td>
<td>Carbon gain function used to optimize stomatal response</td>
<td></td>
<td></td>
</tr>
<tr>
<td>( \theta )</td>
<td>Cost function used to optimize stomatal response</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

aDefault values used for testing the model and the range of values used for testing the effect of these variables on the models output.

bFor the \( D \) response test.

cFor the \( T_L \) response test.

dThis is an exponential curve whereas the others are sigmoidal curves.
The photosynthetic gain function

The water supply function was translated into its corresponding carbon gain function. Figure 1a,b illustrates the step-wise process for the indicated supply function for $P_{\text{seal}} = 0$, $D = 1 \text{kPa}$ and $T_a = 25 \degree C$. In a nutshell, $E$ from the supply function is used to compute leaf temperature ($T_L$) and $D_L$ from energy balance (Fig. 1a, grey dashed $T_L$ and dash-dotted $D_L$ curves). The diffusive conductances of the leaf to water vapour and CO$_2$ ($G_w$, $G_c$, respectively) are obtained from $E$ and $D_L$ (Fig. 1a, solid grey $G_w$ curve). The gross assimilation rate, $A$, is then obtained from $G_c$ and a modelled $A-C_i$ curve (Fig. 1a, green $A$ curve). A normalized gain function ($\beta(P_c)$) is computed to complement the hydraulic cost function ($\theta(P_c)$, Fig. 1b, green $\beta$ curve). The gain function is based on gross assimilation, without subtracting respiration, because in parallel with the cost function, its purpose is to represent the instantaneous gain of opening the stomata. The gross gain provides all energy needs, of which leaf respiration is just one. The leaf temperature, $T_L$ ($\degree C$), was calculated for each supply-function $E$ ($E$ converted to two-sided leaf area basis; Campbell & Norman 1998, Eqs 14.1, 14.3) using the linearized expression:

$$T_L = T_A + \frac{R_{abs} - \varepsilon \sigma T_A^4 - \lambda E}{C_p(\gamma_r + \theta_{ha})},$$

where $R_{abs}$ is absorbed long- and short-wave radiation (W m$^{-2}$), $\varepsilon$ is emissivity (0.97), $\sigma$ is the Stefan–Boltzmann constant ($5.67 \times 10^{-8} \text{W m}^{-2} \text{K}^{-4}$), $T_a$ is mean air temperature in $\degree K$ ($T_a$ is in $\degree C$), $\lambda$ is latent heat of vaporization ($\text{J mol}^{-1}$), $C_p$ is specific heat capacity of dry air at constant pressure (29.3 J mol$^{-1}$ $\degree C^{-1}$), $\gamma_r$ and $\theta_{ha}$ are radiative and heat conductances (mol m$^{-2}$ s$^{-1}$), respectively, for the leaf. The $\theta_{ha} = 0.189 (u/d)^{-0.5}$, where $u$ is mean wind speed (m s$^{-1}$) above the leaf boundary layer, and $d$ is set to 0.72 leaf width in m. Temperature dependence of $\lambda$ and $\gamma_r$ were obtained from Campbell & Norman (1998). Simulations used values in Table 1 unless noted. For constant $T_A$, leaf temperature falls from a maximum at $E = 0$ as transpiration increases (Fig. 1a, grey dashed $T_L$ line).

Leaf temperature was used to calculate $G_w$ by firstly calculating $D_L$. The $D_L$ falls from a maximum at $E = 0$ as transpiration lowers $T_L$ (Fig. 1a, grey dash-dotted $D_L$ line). The $G_w = E/D_L$ (Fig. 1a, grey solid $G_w$ curve), and $G_c = G_w/1.6$. The portion of the curves to the right of the vertical $G_w$ dashed line in Fig. 1a,b corresponds to $E$ above a limit set by a maximum $G_w$ of the leaf (e.g. $G_w$ for maximal stomatal opening at the prevailing boundary layer conductance). The $G_w$ quickly becomes non-limiting as soil dries (e.g. Fig. 1c,d for $P_e = -1 \text{MPa}$) or $D$ increases. Cuticular water loss was assumed zero for present purposes of modelling $G_w$, because it only influences results at or beyond the point of complete stomatal closure.

With $T_L$ and $G_c$ known, gross $A$ was calculated from established photosynthesis models. Rubisco-limited photosynthesis rate, $J_c$, was obtained from (e.g. Collatz et al. 1991; Medlyn et al. 2002):

$$J_c = \frac{V_{\text{max}} \left( C_i - \Gamma^+ \right)}{C_i + K_c \left( 1 + \frac{C_i}{K_c} \right)},$$

where $V_{\text{max}}$ is Rubisco’s maximum carboxylation rate (mol m$^{-2}$ s$^{-1}$), $C_i$ is internal CO$_2$ concentration (Pa), $\Gamma^+$ is the CO$_2$ compensation point (Pa), $K_c$ and $K_o$ are Michaelis–Menten constants for carboxylation and oxygenation, respectively, and $O_a$ is atmospheric O$_2$ concentration (21 000 Pa; $K_c$, $K_o$, $\Gamma^+$ values from Bernacchi et al. 2001).

Electron transport-limited photosynthesis, $J_e$ (mol m$^{-2}$ s$^{-1}$), was obtained from Medlyn et al. (2002):

$$J_e = J \frac{C_i - \Gamma^+}{C_i + 2 \Gamma^+},$$

$$J = \frac{\alpha Q + J_{\text{max}} - \left( \alpha Q + J_{\text{max}} \right)^2 - 4c\alpha QJ_{\text{max}} \right)^{0.5}}{2c},$$

where $\alpha$ is the quantum yield of electron transport (assumed at 0.3 mol photon mol$^{-1}$ e$^{-}$), $Q = \text{PAR photon fluence density} (\mu\text{mol} \text{m}^{-2} \text{s}^{-1})$, $J$ is the actual rate of electron transport (mol m$^{-2}$ s$^{-1}$), $J_{\text{max}}$ is the maximum rate of electron transport (mol m$^{-2}$ s$^{-1}$) and $c$ defines the curvature of the light response curve (0.9).

The gross assimilation rate at a given $C_i$ is the minimum value of $J_e$ and $J_c$. To obtain a smooth $A$ versus $C_i$ curve we used (Collatz et al. 1991):

$$A = \frac{J_e + J_c - \left( \left( J_e + J_c \right)^2 - 4cJ_eJ_c \right)^{0.5}}{2c},$$

where $c'$ is a curvature factor (0.98).

The temperature dependence of $K_o$, $K_c$ and $\Gamma^+$ relative to 25 $\degree C$ was modelled as in Bernacchi et al. (2001) and Medlyn et al. (2002). The temperature dependence of $J_{\text{max}}$ and $V_{\text{max}}$ relative to 25 $\degree C$ ($J_{\text{max}25}$ and $V_{\text{max}25}$, respectively) was modelled using Leuning (2002) (his equation 1 with parameters from his Table 2). We assumed $V_{\text{max}25}$ and $J_{\text{max}25}$ co-varied, using $J_{\text{max}25} = V_{\text{max}25} \cdot 1.67$ (Medlyn et al. 2002).

The only unknown variable in Eqn 8 is $C_i$. However, we know $G_c$ from the supply function, which gives a second equation for $A$:

$$A = \frac{G_c (C_a - C_i)}{P_{\text{atm}}},$$

where $C_a$ is atmospheric CO$_2$ concentration (40 Pa) and $P_{\text{atm}}$ is atmospheric pressure (101.3 kPa). We set Eqs 9 and 8 equal to each other and solved for $C_i$ thereby obtaining $A$. Both $C_i$ and $A$ rise steeply with $G_w$ before approaching saturation (Fig. 1a, grey dashed $C_i$ curve and green $A$ curve for parameter values listed in Table 1).

A normalized photosynthetic gain function ($\beta(P_c)$) was calculated as

$$\beta(P_c) = \frac{A(P_c)}{A_{\text{max}}},$$

where $A$ is evaluated at $P_c$ and $A_{\text{max}}$ is the instantaneous maximum $A$ over the full $P_c$ range from $P_c = P_e$ to $P_c = P_{\text{crit}}$ (not the
biochemical $A_{\text{max}}$). The gain function rises steeply from $\beta = 0$ at $P_c = P_e$ as stomata open before flattening to $\beta = 1$ as $P_c$ becomes more negative and photosynthesis saturates (Fig. 1b, green $\beta$ curve). Like the $\theta(P_e)$ cost function, the gain function is normalized by the extremes, making it dimensionless, and relevant only to the moment in time for which it is computed.

It is important to know that the family of $f(P_e)$ curves in Fig. 1a,b $[E(P_e), T_1(P_e), D_1(P_e), G_w(P_e), C_i(P_e), A(P_e), \theta(P_e), \beta(P_e)]$ represent steady-state values at a fixed instant where root zone $P_o$, atmospheric $D$, air temperature ($T_a$), wind speed ($u$) and light level ($Q$) are frozen in time. The plant can only occupy one stable point on this theoretical constellation of possibilities. At the next time step, gradual shifts in soil and air moisture, temperature, windspeed and light create a new set of possibilities, only one of which the leaf will 'target' via its stomatal response (assuming stomata keep pace with typically gradual changes). Figure 1c,d shows, for example, how these functions shift when $P_s$ drops to $-1$ MPa. If a simple rule that approximated the presumably adaptive stomatal response can be found, then it becomes possible to anticipate where the plant regulates itself on these gradually shifting curves, assuming approximately steady-state conditions.

**Instantaneous profit maximization**

Wolf et al. (2016) pose the optimization criterion that at each instant in time, the stomata regulate canopy gas exchange and pressure to achieve the maximum profit, which is the maximum difference between the normalized photosynthetic gain and hydraulic cost functions:

$$\text{Profit}_{\text{max}} = [\beta(P_e) - \theta(P_e)]_{\text{max}}.$$  \hspace{1cm} (11a)

The maximization is achieved when:

$$\frac{\partial \beta}{\partial P_e} = \frac{\partial \theta}{\partial P_e}. \hspace{1cm} (11b)$$

Note that $\beta$ and $\theta$ can be expressed as functions of $G_w$ instead of $P_e$ because of the coupling evident in Fig. 1. Figure 1b shows the $\beta-\theta$ curve and its maximum (black curve), which coincides with equal gain and cost derivatives (Fig. 1b, green and blue tangent lines to their respective curves). Instantaneous profit maximization assumes a ‘use it or lose it’ reality with regards to available soil water. Any more conservative water use strategy would backfire when soil water is not safe from competitors (i.e. instantaneous optimizers), drainage or surface evaporation. Although modelling optimization avoids specifying mechanism, $\beta$ and $\theta$ are determined by leaf-level phenomena: $A$ for $\beta$, and $\partial E/\partial P_c$ for $\theta$. Plants can sense their photosynthetic status and water balance (Paul & Foyer 2001; Tombesi et al. 2015), and hence potentially how both change in response to active control of $G_w$ and $E$. The steady-state assumption represents the sustainable baseline $\beta$ and $\theta$. This is most appropriate for middle of day gas exchange, which is generally a good predictor of daily totals (e.g. von Allmen et al. 2015).

Because the gain function accelerates more quickly from zero and reaches 1 sooner than the cost function (Fig. 1b, green versus blue curves), their maximum difference occurs at a unique intermediate $P_e$ (Fig. 1b, black $\beta-\theta$ curve), which yields the corresponding solutions for actual $E, G_w, A, G_c, C_i, T_1$, and $D_1$ at that instant (Fig. 1, dashed arrows from maximum to open symbols on curves in (a)).

As environmental conditions shift, so does the optimum. The influence of drier soil ($P_s = -1$ MPa) is shown in Fig. 1c,d. The cost and gain functions are reset to start from 0 at $P_e = P_s$ and rise to 1, but they rise from a more negative $P_s$. The rise of the gain function is not materially altered (only via changes in $T_1$) because we assumed no direct effect of $P_e$ on $A$. However, the cost function rises more steeply because it is computed from the more curved part of the supply function where more cavitation is occurring. The rapidly rising cost results in a smaller optimal soil-canopy $\Delta P$, and a lower optimal $G_w$. The Fig. 1 example was computed from a sigmoidal vulnerability curve ($b = 2, c = 3$). As explored under ‘model performance’ the shape of the vulnerability curve influences how $P_c$ changes the cost function shape, and how the optimal pressure drop and $G_w$ change with drying soil.

The optimal solution also depends on $D, T_A, C_a$ and light. These environmental variables influence the optimum by changing the shape of the gain function, as discussed under ‘model performance’. When conditions flatten the gain function (e.g. high $D$, low $C_a$, high $T_A$; Fig. 2a, dashed green curve), the optimum shifts to more negative $P_c$ (dashed black curve) driving an increase in the optimal soil-canopy pressure drop.

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**Table 2.** Ball–Berry–Leuning Model fits (BBL; Eqn 12; Leuning 1995) to leaf diffusive conductance ($G_w$) predicted from profit maximization (as plotted in Fig. 8). Means and standard error (in parentheses) given for $n > 1$ simulations

<table>
<thead>
<tr>
<th>Response</th>
<th>$n$</th>
<th>$r^2$</th>
<th>$a'$</th>
<th>$D_o$ (kPa)</th>
<th>$G_w$ (mol s$^{-1}$ m$^{-2}$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>$D_1^+$ (Fig. 4)</td>
<td>6</td>
<td>0.99738(0.000065)</td>
<td>14.0(0.91)</td>
<td>0.64(0.067)</td>
<td>0.036(0.0063)</td>
</tr>
<tr>
<td>$D_1$ (Fig. 7)</td>
<td>11</td>
<td>0.99968(0.000038)</td>
<td>27.5(0.37)</td>
<td>0.213(0.0054)</td>
<td>0.0673(0.00127)</td>
</tr>
<tr>
<td>$C_i^+$ (Fig. 7)</td>
<td>5</td>
<td>0.988(0.0038)</td>
<td>36.0(0.00093)</td>
<td>0.126(0.0037)</td>
<td>0.110(0.0038)</td>
</tr>
<tr>
<td>$Q^+$ (Fig. 5)</td>
<td>1</td>
<td>0.91</td>
<td>79.71</td>
<td>0.04</td>
<td>0.16</td>
</tr>
<tr>
<td>$T_1^+$ (Fig. 5)</td>
<td>1</td>
<td>0.12</td>
<td>8.59</td>
<td>0.16</td>
<td>0.22</td>
</tr>
<tr>
<td>$P_c^+$ (Fig. 6)</td>
<td>6</td>
<td>0.9416(0.00260)</td>
<td>260(165)</td>
<td>0.09(0.034)</td>
<td>-0.0132(0.00212)</td>
</tr>
</tbody>
</table>

*aLeaf-air vapour pressure deficit.
*bAmbient CO$_2$ concentration.
*cPhotosynthetically active radiation.
*dLeaf temperature.
*eSoil water potential.

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Longer-term optimization of photosynthetic and hydraulic parameters

Employing the instantaneous optimization scheme to solve for plant gas exchange reveals a second scale of optimal coordination between photosynthetic capacity ($V_{\text{max}25} = J_{\text{max}25}/1.67$), maximum hydraulic capacity (maximum soil-canopy hydraulic conductance, $k_{\text{max}}$ expressed per leaf area), and maximum diffusive conductance ($G_{\text{max}}$). Assuming firstly that $G_{\text{max}}$ is not limiting, if $k_{\text{max}}$ is set too low relative to $V_{\text{max}25}$, the instantaneously optimal $E$ and $G_2$ are low, and $G_2$ limits the optimum $A$ (Fig. 3a, solid $A$ curves for $V_{\text{max}25} = 25$ versus $150 \mu\text{mol s}^{-1}\text{m}^{-2}$) even under the most favourable conditions.

**Figure 2.** Effects of environment and plant on the cost ($\theta$, blue) and gain ($\beta$, green) functions and their difference ($\beta-\theta$, black). (a) The gain function shifts in the direction of the green arrow if there is an increase in vapour pressure deficit ($D$), air temperature ($T_a$), or below photosynthetic optimum), or maximum carboxylation rate ($V_{\text{max}}$), or a decrease in ambient CO$_2$ concentration ($C_a$). This results in a shift of the optimum (black arrows) in the direction of the red arrow. The cost function is not affected by changes in these variables. (b) The cost function shifts in the direction of the blue arrow as cavitation resistance increases, resulting in an shift of the optimum (black arrows) in the direction indicated by the red arrow. The gain function also shifts with the soil-canopy vulnerability curve change because of differences in leaf temperature. (Fig. 2a, red arrow, dashed vertical arrow). When conditions steepen the gain function (e.g. low $D$, high $C_a$, low $T_a$; Fig. 2a solid green curve), the optimum results in less negative $P_c$ (solid black curve) and a smaller soil-canopy pressure drop (Fig. 2a, solid vertical arrow).

The key plant traits that influence the optimum include the vulnerability curve (Weibull $b$, $c$ parameters), the maximum soil-canopy hydraulic conductance ($k_{\text{max}}$) and leaf diffusive conductance ($G_{\text{max}}$), and the photosynthetic capacity ($V_{\text{max}25}$). More vulnerable xylem creates a faster rise in the cost function and forces a less negative optimal $P_c$ (Fig. 2b, solid curves for vulnerable xylem versus dashed for resistant). A higher $k_{\text{max}}$ and $G_{\text{max}}$ increase $E$ and $G_2$ for a given optimal $P_c$. A greater $V_{\text{max}25}$ creates a slower rise in the gain function and drives optimal $P_c$ to a more negative value (Fig. 2a, dashed curves; see also Fig. S1d). As described next, the model predicts that these plant traits should be highly coordinated.

**Figure 3.** Optimal coordination among soil-canopy maximum hydraulic conductance ($k_{\text{max}}$), maximum diffusive conductance ($G_{\text{max}}$) and photosynthetic capacity ($V_{\text{max}25}$). (a) Instantaneous optimal gross assimilation rate ($A$) for two maximum carboxylation rates ($V_{\text{max}25}=25 \mu\text{mol s}^{-1}\text{m}^{-2}$ (25, solid grey curve) and $150 \mu\text{mol s}^{-1}\text{m}^{-2}$ (150, solid black curve)) calculated for different values of $k_{\text{max}}$. The leaf internal CO$_2$ concentrations ($C_i$) corresponding to these instantaneous optimum assimilation rates are also represented for $A_{25}$ (solid grey curve) and $A_{150}$ (broken black curve). Optimal $k_{\text{max}}$ for each $V_{\text{max}25}$ (vertical arrows) is determined when the $C_i/C_a = 0.7$ (intersection of $C_i$ curves with black dotted $C_i/C_a = 0.7$ line; $C_a = 40 \text{kPa}$). (b) The optimal $k_{\text{max}}$ (black curves) increases with $V_{\text{max}25}$ and also increases with more vulnerable xylem (as indicated by higher $P_{50}$, which is the xylem pressure at which 50% of conductivity loss is reached). The Weibull parameters $[b,c]$ for the three curves represented were $[1,3]$ for $P_{50} = -0.88 \text{MPa}$, $[2,3]$ for $P_{50} = -1.77 \text{MPa}$ and $[3,3]$ for $P_{50} = -2.70 \text{MPa}$. The optimal $G_{\text{max}}$ increases with $V_{\text{max}25}$ (grey line), but does not change with xylem vulnerability.
(Fig. 3a assumes full sunlight, \( D = 1 \) kPa, \( P_{\text{soil}} = 0 \) MPa, \( T_a = 25 ^\circ \text{C} \)). Greater \( k_{\text{max}} \) causes \( G_c \) to increase, allowing the instantaneous optimum \( A \) to rise and saturate for a given \( V_{\text{max25}} \) setting (Fig. 3a, solid \( A \) curves). The rise along a given optimal \( A \) curve is paralleled by a rise in \( C_i \) (Fig. 3a, dashed \( C_i \) curves accompanying respective \( A \) curves). Over the long term, a plant should invest in sufficiently large \( k_{\text{max}} \) to nearly saturate the instantaneous optimum \( A \) under favourable conditions. Too low \( k_{\text{max}} \) would fail to realize maximum photosynthetic potential; too high \( k_{\text{max}} \) would be wasted on negligible return. The theory predicts near saturated optimal \( A \) at a \( C_i/C_a \) ratio of ca. 0.7 (Fig. 3a, dotted \( C_i/C_a = 0.7 \) line; \( C_a = 40 \) Pa), which is also what is typically observed in C3 plants under favourable conditions (Wong et al. 1979; Hetherington & Woodward 2003; Prentice et al. 2014). In this paper, the interest is in modelling plant responses to environmental variables, so we used this \( k_{\text{max}} \) versus \( V_{\text{max}} \) coordination (plotted in Fig. 3b, black optimal \( k_{\text{max}} \) curves) to simplify parameterization (\( k_{\text{max}} \) is set to achieve \( C_i = 28 \) Pa at \( D = 1 \) kPa, \( P_i = 0 \) MPa, \( T_a = 25 ^\circ \text{C} \)). Similarly, we chose a \( G_{\text{max}} \) that was sufficiently high so as not to limit optimal \( A \) under favourable conditions, but not overly high. We used \( G_w \) at \( D = 0.25 \) kPa as our \( G_{\text{max}} \) setting (Fig. 3b, \( G_{\text{max}} \) curve).

The optimal \( k_{\text{max}} \) also depends on the vulnerability of the xylem to cavitation, with more vulnerable xylem requiring higher \( k_{\text{max}} \) to achieve \( C_i/C_a = 0.7 \) (Fig. 3b, \( k_{\text{max}} \) curves for sigmoidal curves [Weibull \( c = 3, b = 1, 2, 3 \); pressures at 50% loss of conductivity, \( P_{\text{soil}} \) shown in Fig. 3b]). The reason for this is that cavitation at modest \( P_i \) makes the hydraulic cost (\( \theta \)) rise faster (Fig. 2b, solid blue curve for vulnerable xylem), restricting the optimal soil-canopy \( \Delta P \) (vertical solid arrow for solid black curve). Low \( \Delta P \) means low \( E \) and \( G_c \). Increasing \( k_{\text{max}} \) does not change the optimal \( \Delta P \) much, but it does increase \( E \) and \( G_c \), which allows optimal \( A \) to rise and \( C_i/C_a \) to reach 0.7. The \( G_{\text{max}} \) corresponding to \( C_i/C_a = 0.7 \) does not depend on vulnerability (Fig. 3b, single \( G_{\text{max}} \) curve).

**MODEL PERFORMANCE**

**Responses to environment**

In this section, the responses of the optimization model to various environmental factors are examined. We assumed the coordination of \( V_{\text{max25}}, k_{\text{max}} \) and \( G_{\text{max}} \) as described in the previous section. For each environmental factor, all other parameters were held constant at default values (Table 1) except as noted. We examine the \( G_w \) and \( P_c \) sensitivity to \( V_{\text{max25}} \) settings first (\( V_{\text{max25}} = 25 \) versus 150 \( \mu \text{mol} \cdot \text{s}^{-1} \cdot \text{m}^{-2} \)), and then to vulnerability curve settings (at \( V_{\text{max25}} = 100 \) \( \mu \text{mol} \cdot \text{s}^{-1} \cdot \text{m}^{-2} \)). For vulnerability curves, we use sigmoidal curves (Weibull \( c = 3 \), varying \( b \) from 1 to 3) and also explore the change in curve shape from sigmoidal \((c = 3)\) to exponential \((c = 1)\) while holding \( b = 2 \). We compare the carbon versus water optimization solution with the purely hydraulic solution from the model of Sperry et al. 2016 for the same settings, using Eqn 3 instead of Eqn 11 to locate the plant on the \( E(P_c), A(P_c) \), and associated family of \( f(P_c) \) functions (Fig. 1a). In a concluding section, we evaluate the fit of the empirical BBL model for each environmental response.

**Leaf-to-air vapour pressure deficit, \( D_L \)**

To obtain the response to \( D_L \), we varied the atmospheric \( D \) at a constant \( T_A \) = 30 °C (maximum \( D = 4.26 \) kPa), and \( P_t = 0 \). Owing to generally higher \( T_A \), this yielded maximum \( D_L \) of ca. 4.5 kPa. Higher \( D_L \) flattened the \( G_w(P_c) \) curve (i.e. the grey \( G_w \) curve in Fig. 1a), resulting in a lower optimal \( G_w \) and the typical closure response (Fig. 4a). Closure started from an initial \( G_w \) that depended on the \( V_{\text{max25}} \) setting as described in the previous section. Higher \( D_L \) was also associated with a gradual decline in \( P_c \) (Fig. 4b). This happened because the flatter \( G_w(P_c) \) curve also flattened the gain function, which makes optimal \( P_c \) more negative (i.e. as illustrated by the dashed curves in Fig. 2a, see Fig. S1a for a specific example).

The general closure response was similar to that of the hydraulic model, although with two subtle differences. The hydraulic model predicted a smooth transition from \( G_{\text{max}} \) versus the sharp one for optimization (Fig. 4a, b), best seen for solid \( V_{\text{max25}} = 150 \) curve. This difference may be trivial, however, because \( G_{\text{max}} \) is unlikely to be limiting under typical \( D_L \). The hydraulic model also predicted slightly more closure at high \( D_L \), corresponding to its assumption of achieving perfectly isohydric \( P_c \) (Fig. 3b, grey curves). This differs from the aforementioned quasi-isohydric response of the optimization scheme, with \( P_c \) creeping to more negative values at high \( D_L \) (Fig. 3b, black curves). In general, however, \( P_c \) values were in a similar range for the two schemes.

The \( G_w \) response to \( D_L \) was not sensitive to vulnerability to cavitation for the sigmoidal curves tested (Fig. 4c, solid black curve for \( b = 1, 3 \), \( c = 3 \)), and this was true for the hydraulic model as well (Fig. 4c, grey curve). The insensitivity results from the insensitivity of \( G_{\text{max}} \) to sigmoid vulnerability achieved via \( k_{\text{max}} \) coordination (Fig. 3b). However, for the exponential vulnerability curve, more closure was predicted for all \( D_L \) (Fig. 4c, dashed black curve for \( b = 2, c = 1 \)), similar to the hydraulic model prediction (Fig. 4c, dashed grey curve). In both cases, the result is attributable to the steeper initial rise in the cost function associated with cavitation of highly vulnerable xylem at the start of the exponential vulnerability curve (Fig. S2a).

The optimal \( P_c \) became significantly more negative in response to greater Weibull \( b \) (greater cavitation resistance) at all \( D_L \) for the sigmoidal curves (Fig. 4d, solid black curves). This owes to the delayed rise in the cost function with greater sigmoid resistance (as illustrated by dashed curves in Fig. 2b; see also Fig. S1f). The \( P_t \) for the exponential curve was relatively modest (Fig. 4d, dashed black curve, \( b = 2, c = 1 \)), again because of the steeper initial rise in the cost function for an exponential versus a sigmoidal curve (Fig. S2a). The hydraulic model predicted similar \( P_c \) responses to vulnerability, but with perfect isohydry at high \( D_L \) (Fig. 4d, grey solid (\( b \) varying) and dashed (\( b = 2, c = 1 \)) curves).

**Temperature and light, \( T_A, T_L, Q \)**

The main effect of temperature on \( G_w \) and \( P_c \) is via its influence on \( D_L \). However, there was a direct effect of leaf temperature revealed by holding \( D_L \) constant. We show just one example, © 2016 John Wiley & Sons Ltd, Plant, Cell and Environment
keeping $D_L$ constant at ca. 1.5 kPa by varying $D$, and setting $k_{\text{max}}$ to its optimum at $T_A = 25 ^\circ \text{C}$ and $V_{\text{max}} = 100 \mu \text{mol s}^{-1} \text{m}^{-2}$. In the optimization model, $G_w$, $A$, $E$, and $P_c$ all respond to temperature, rising to a maximum before falling at high $T_L$ (Fig. 5a, solid black $G_w$ curve, dashed black $A$ curve). The response is caused by the temperature-induced shift in the gain function, from saturation at modest $P_c$ under cool conditions (e.g. represented by the solid green curve in Fig. 2a; see Fig. S1b for specific example) to saturation at more negative $P_c$ under optimal warmth (dashed green curve in Fig. 2a). The hydraulic model shows no temperature response of $G_w$ (nor $E$ or $P_c$; Fig. 5a, solid grey $G_w$ line) because its $P_c$ solution is independent of temperature (Eqn 3). The $A$ response, however, is similar to the optimization prediction because the $A(P_c)$ curve is identical between models (Fig. 5a, dashed grey $A$ curve).

The optimization model also responds to light, predicting stomatal closure as $Q$ (PAR) falls to zero (Fig. 5b). The exact $G_w$ by $Q$ trajectory depends on how $D$, $T_A$, $u$ and $R_{\text{abs}}$ co-vary with $Q$. For the sake of isolating the light response, we held $D$, $T_A$ and $u$ constant, but allowed $R_{\text{abs}}$ to fall linearly with $Q$ from the default 740 W m$^{-2}$ to earth’s black body radiation at $Q=0$. The optimization model predicts stomatal closure because lower light causes $A$ to saturate at less negative $P_c$, which steepens the gain function and results in a less negative optimal $P_c$. In contrast, the hydraulic model does not predict stomatal closure under low light, because stomata do not respond to $A$. The $A$ trajectory is similar in both models, falling with $Q$ according to Eqn 7 in both models.

### Soil water potential, $P_s$

With $D$ held constant at 1 kPa ($T_A = 25 ^\circ \text{C}$), the optimization scheme predicted stomatal closure in response to $P_s$ (Fig. 6a). While some of the closure response is associated with a slight, but inevitable increase in $D_L$ because of less transpirational cooling (from $D_L = 1.3$ to ca. 1.65 kPa), closure was predicted even if $D_L$ was held constant (by manipulating $D$). The $P_c$-induced closure resulted from two factors: the generally flatter $E(P_c)$ trajectory caused by dry soil (e.g. compare blue $E$ curves in Fig. 1a versus 1c), and the faster rise in the cost function (e.g. compare blue $\theta$ curves in Fig. 1b versus 1d; see also Fig. S1e), which restricts the soil-canopy pressure drop. The closure response starts from higher $G_w$ with greater $V_{\text{max}}$, consistent with Fig. 4a for the $D_L$ response. If $V_{\text{max}}$ was down-regulated (e.g. Limousin et al. 2013) with $P_s$ (to maintain $C_i/C_e = 0.7$), closure was accelerated slightly (Fig. 6, down-regulated curve for initial $V_{\text{max}} = 150 \mu \text{mol s}^{-1} \text{m}^{-2}$). The hydraulic model (Fig. 6a, grey curves) predicted somewhat more gradual closure than the optimization scheme. Both scenarios predicted nearly complete closure at a similar $P_s$ (ca. $-3 \text{MPa}$ for the Weibull $b = 2, c = 3$ default vulnerability curve; $P_{\text{crit}}$ ca. $-4 \text{MPa}$).

The closure response to $P_s$ was associated with a reduction in $P_c$, that was similar regardless of $V_{\text{max}}$ setting (Fig. 6b, solid black curve). Downregulation of $V_{\text{max}}$ with $P_s$ (Fig. 6b) restricted the drop of $P_c$ in keeping with the accelerated closure response. A similar restriction on $P_c$ was also seen for the hydraulic model (Fig. 6b, solid grey curve). Both models predicted a gradual reduction in soil-canopy $\Delta P$ as soils dried. This $\Delta P$ reduction resulted from the steeper cost associated with
more negative $P_s$ for the default sigmoidal vulnerability curve (as illustrated in Fig. 1b,d; see also Fig. S1e).

Vulnerability to cavitation had a major influence on the stomatal sensitivity to $P_c$. More resistant sigmoidal curves relaxed the cost function (dashed blue line in Fig. 2b; see Fig. S1e for specific example) and resulted in more gradual closure that extended gas exchange to more negative $P_c$ (Fig. 6c, solid black curves). Altering a sigmoidal curve ($b = 2$, $c = 3$) to an exponential one ($b = 2$, $c = 1$) caused more even gradual closure and extension to even more negative $P_c$ (Fig. 6c, dashed black curve). As noted before, exponential curves produce steep cost functions in wet soil because of lots of initial cavitation (Fig. S2a). The long, flat tail of the exponential curve ($P_{crit}$ of ca. −17 MPa) results in a relatively less steep cost function, and hence relatively less closure (and more negative $P_c$) than a sigmoidal curve. In all cases, the $G_w$ response to vulnerability curves was similar to the hydraulic model (Fig. 3c, solid grey curves for sigmoidal, dashed grey for exponential shape).

The $P_c$ regulation paralleled the $G_w$ trend. More resistant sigmoidal curves resulted in more gradual reduction in the soil-canopy Δ$P$ extending to more negative $P_c$ (Fig. 6d, solid black curves), a trend very similar to the hydraulic model (Fig. 6d, solid grey curves). The exponential curve ($b = 2$, $c = 1$) caused a more restricted Δ$P$ in wet soil, but a gradual increase in Δ$P$ with more negative $P_c$ (Fig. 6d, dashed black curve). Beyond the scale shown in Fig. 6d, the Δ$P$ diminished again, but gas exchange at that point is negligible (Fig. 6c). This exponential Δ$P$ response results from the relatively steep cost function in wet soil that relaxes at intermediate $P_s$ (Fig. S2). The hydraulic model predicts near constant Δ$P$ for the exponential curve (Fig. 6d, dashed grey curve).

### CO2 response, $C_a$

We computed the CO2 response by holding $V_{max25}$ constant (100 μmol s$^{-1}$ m$^{-2}$), setting $T_0$ to 25 °C, and allowing $G_{max}$ to be unlimited (to detect the maximum opening response). The optimization scheme predicted stomatal opening and more negative $P_c$ in response to low atmospheric $C_a$ (<40 Pa), and closure with $P_c$ moderation under high $C_a$ (>40 Pa; Fig. 7). Low CO2 caused opening because it made the gain function saturate at more negative $P_c$, thus making optimal $P_c$ more negative, and increasing the optimal $E$ and $G_w$ (i.e. the response represented by the dashed green and black curves in Fig. 2a; see Fig. S1c for an example). High CO2 caused closure because it caused the gain function to saturate at less negative $P_c$, making the optimal $P_c$ less negative, along with lower $E$ and $G_w$ (the solid green and black curves in Fig. 2a). Higher $V_{max25}$ and higher temperature (up to the optimum) created a greater CO2 response than lower $V_{max25}$ and temperature (responses not shown).

The CO2 response was also greatest at low $D$ (Fig. 1a,b) and less negative $P_s$ (Fig. 1c,d) because these conditions promoted generally high $G_w$, and hence greater scope for the CO2 response. High $D$ and negative $P_s$ suppressed $G_w$ and the CO2 response. Increasing the sigmoidal resistance to cavitation had no effect on the wet soil CO2 response (i.e. the responses in Fig. 7a,b), but decreased the attenuation in CO2 response with $P_s$ (i.e. reduced the rate at which the CO2 response dropped with $P_s$ in Fig. 7c,d).

### Comparison to Ball–Berry–Leuning (BBL) model

The BBL model (Leuning 1995) empirically relates $G_w$ (mol s$^{-1}$ m$^{-2}$) to $A$ (μmol s$^{-1}$ m$^{-2}$), $D_L$, and $C_{a}$:

$$G_w = G_o + \frac{a' A}{(C_a - \Gamma^*)^{1 + \frac{D_o}{\Gamma^*}}}$$

where $C_{a}$ is the CO2 concentration at the leaf surface (set to $C_{a}$, μmol mol$^{-1}$, $\Gamma^*$ in same units), and $G_o$ (mol s$^{-1}$ m$^{-2}$), $a'$ (dimensionless) and $D_o$ (kPa) are fitted coefficients. The BBL model provided near perfect fits to the optimization $G_w$ for both the $D_L$ and $C_{a}$ responses from Figs 4 and 7 (Fig. 8a, b; $r^2 \approx 1$). Best-fit coefficients ($a'$, $G_o$, $D_o$; Table 2) were relatively stable. The light response from Fig. 5b was fit less well.
Figure 6. Diffusive vapour conductance ($G_w$) and xylem canopy pressure ($P_c$) responses to soil water potential ($P_s$) of the optimization model (black curves) versus the Sperry et al. (2016) hydraulic model (grey curves). (a) $G_w$ response to $P_s$ for both models for two maximum carboxylation rates, $V_{\text{max25}} = 25 \mu\text{mol s}^{-1} \text{m}^{-2}$ (dashed curves) and $V_{\text{max25}} = 150 \mu\text{mol s}^{-1} \text{m}^{-2}$ (solid curves). Dash-dotted ‘downregulated’ curve corresponds to reduction in $V_{\text{max25}}$ from 150 $\mu\text{mol s}^{-1} \text{m}^{-2}$ as required to maintain internal CO$_2$ at 70% of ambient. (b) $P_c$ response to $P_s$ (the response for both $V_{\text{max25}}$ values was equal; dash-dotted represents downregulated $V_{\text{max25}}$). (c) $G_w$ and (d) $P_c$ response to $P_s$ for both models for different vulnerability curves (VCs) as determined by the Weibull $[b,c]$ parameters (sigmoidal VCs [1–3,3], solid curves; exponential VCs [2,1], dashed curves). All other parameters are given in Table 1. The dash-point line represents the 1:1 relation between $P_c$ and $P_s$.

Figure 7. Diffusive conductance ($G_w$) and canopy xylem pressure ($P_c$) responses to different atmospheric CO$_2$ concentrations ($C_a$). (a) Percent $G_w$ difference relative to $G_w$ at $C_a = 40 \text{Pa}$ for different air vapour pressure deficits ($D$). (b) Percent $P_c$ difference relative to $P_c$ at $C_a = 40 \text{Pa}$ for different air vapour pressure deficits ($D$). (c) Percent $G_w$ difference relative to $G_w$ at $C_a = 40 \text{Pa}$ for different soil water potentials ($P_s$). (d) Percent $P_c$ difference relative to $P_c$ at $C_a = 40 \text{Pa}$ for different soil water potentials ($P_s$).

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(Fig. 8c; Table 2; $r^2 0.91$), with BBL predicting more gradual closure in low light. The temperature response was poorly fit (Fig. 8c; Table 2; $r^2 0.12$) with BBL over-predicting $G_w$ at low temps and under-predicting at high. However, this simulation represents an unusual challenge to BBL in that it is unlikely in nature to have leaf temperature varying independently of $D_L$. The BBL was not intended to capture the $P_s$ response, which is reflected in its poor fit to the Fig. 6 simulations (Fig. 8d, Table 2). Although the $r^2$ averaged 0.94, there was consistent non-linearity because BBL under-predicted the rate of stomatal closure with $P_s$. The $a'$ coefficient was quite variable across the $P_s$ simulations, and $G_w$ was consistently negative (Table 2).

**DISCUSSION**

Our purpose was to present the rationale and quantitative proof of concept for a novel and synthetic model for stomatal responses at the leaf scale. The profit-maximizing scheme efficiently predicted a wide range of stomatal ($G_w$) and xylem pressure ($P_c$) responses to environmental factors (Figs 3–7) without recourse to ad hoc empirical coefficients. The instantaneous $E(P_c)$ and $A(P_c)$ functions (Fig. 1a,c, blue $E$ and green $A$ curves) are calculated from established hydraulic and biochemical processes initialized by measurable traits (Table 1). They represent the full spectrum of steady-state water-for-carbon exchange options available at a given instant. The supply $E(P_c)$ function is a defensible proxy for the increasing cost of losing more water: every additional increment in stomatal conductance sooner or later requires an ever-increasing drop in $P_c$, owing to ever-declining canopy hydraulic conductance, which accelerates the approach to certain desiccation at $E_{crit}$. Clearly, either extreme of the $A(P_c)$ and $E(P_c)$ exchange spectrum is non-adaptive, and the plant should be somewhere in the middle. The optimization criterion is straightforward: at a given instant, stomata should maximize the difference between photosynthetic gain and hydraulic cost. Both gain and cost metrics are normalized to zero at stomatal closure and 1 at the maximum over the hydraulically permissible range of stomatal opening for that instant. This simple algorithm predicts a host of plant responses (e.g. $E$, $A$, $G_w$, $P_c$, $T_L$, $C_i$) to a combination of plant and environmental factors (e.g. $k_{max}$, $V_{max25}$, cavitation vulnerability, leaf size, $P_w$, $D$, $T_A$, $C_a$, $u$, $Q$).

The general congruence between the optimization scheme and the hydraulics-only approach (Eqn 3; Sperry & Love 2015; Sperry et al. 2016) results from the common use of the $E(P_c)$ derivative ($k_c$) as the key model factor that constrains stomatal opening. The largest qualitative difference is that optimization predicts non-isohydric $P_c$ response to increasing $D_L$, which is arguably more realistic than the strict $D_L$ isohydry predicted by the hydraulic model (Fig. 4b,c). Nevertheless, the hydraulic model appears to explain much of the variation in stomatal responses ($G_w$ and $P_c$) to $D$ and $P_v$ (Sperry et al. 2016), and should be useful when the additional photosynthetic parameters required for the optimization scheme are...
unavailable, and CO₂ and light do not vary substantially. All of its advantages in capturing the isohydric-to-anisohydric spectrum (e.g. Fig. 6d; and see Sperry et al. 2016), and the coupled responses to \( D_L \) and \( P_s \) (Figs 4 & 7), carry over in the optimization model. However, the optimization model captures the most complete suite of stomatal responses because \( G_w \) responds to \( A \). This allows it to predict additional responses to \( T_A \), \( Q \) and \( C_w \) (Figs 5 & 7).

The comparison to the Ball–Berry–Lueuning (Leuning 1995) model (BBL) represents a ‘zero-order’ test of the optimization model. The BBL fit was essentially perfect for the stomatal response to \( D_L \) and \( C_w \) (Figs 4 & 7). This result was anticipated by the BBL form of theoretical derivations for profit maximization (Wolf et al. 2016). The BBL congruency suggests that the trends in Figs 4 (closure at high \( D_L \)) and 7 (opening at low \( C_w \), closure at high \( C_w \)) are quantitatively as well as qualitatively consistent with observations. The advantage of the optimization approach over BBL (or other empirical models) is the absence of \( ad \) \( hoc \) fitting parameters (e.g. Table 2) and its basis in trait and process. Even more importantly, the optimization model applies equally well to dry soil (e.g. Fig. 6a,c). The BBL model lacks any parameter for capturing the \( G_w \) response to drying soil (Eqn 12; Darmour et al. 2010), and under-predicts stomatal closure relative to the optimization model (Fig. 8d). This critical defect is often patched up in ecosystem models by the addition of more \( ad \) \( hoc \) functions and coefficients (Jarvis 1976; Powell et al. 2013). But the optimization model provides a simpler and more powerful alternative. Its integration of photosynthesis and hydraulics predicts not only gas exchange and energy balance, but the accompanying water relations and hydraulic status. As the rapidly growing literature on drought induced tree mortality suggests, metabolic, temperature and hydraulic stresses are inextricably intertwined during drought (McDowell et al. 2008; Rowland et al. 2015; Anderegg et al. 2016). Models need to represent their integration to best predict responses to environmental change (McDowell et al. 2013).

Additional evidence for the optimization model comes from its prediction of a tightly coupled coordination between \( k_{max}, G_{max} \) and \( V_{max25} \) (Fig. 3). This is consistent with an abundance of data showing a positive relationship between \( k_{leaf} \) and \( V_{max} \) (Clearwater & Meinzer 2001; Brodribb et al. 2002; Brodribb et al. 2005; Brodribb et al. 2007; Campanello et al. 2008; Brodribb 2009; Brodribb & Feild 2010; Limousin et al. 2013; Novick et al. 2016). The coordination between hydraulic and photosynthetic capacity emerges from the assumption that \( C_i/C_a \) is maintained at a set value under favourable conditions. A constant \( C_i/C_a \) target was also proposed as a carbon-water transport optimization criterion by Prentice et al. (2014), and previous modelling has demonstrated its theoretical link to plant hydraulic properties (Katul et al. 2003). The optimal \( k_{max} \) settings also correspond to leaf area-specific hydraulic conductances within the measured range (5–65 mmol s⁻¹ m⁻¹ MPa; assuming leaves are 25% of plant resistance at full hydration; Sack & Tyree 2005). The further prediction that \( k_{max} \) should increase with vulnerability to cavitation (Fig. 3b) is consistent with generally observed trends (Gleason et al. 2015). Interestingly, however, this trend is predicted independently of any safety versus efficiency trade-off at the xylem level. Instead, it emerges from vulnerable xylem limiting the soil-canopy \( \Delta P \), thus requiring higher \( k_{max} \) to achieve the \( G_w \) required to keep \( A \) and \( C_i \) at optimal levels (Fig. 3a).

Our optimization criterion, that of instantaneously maximizing carbon gain (\( \beta \)) minus hydraulic cost (\( \partial \) Eqn 11; Wolf et al. 2016), is importantly different from the Cowan–Farquhar maximization of carbon gain for a fixed amount of water loss. The \( \partial E/\partial A = \lambda ' \) target for stomatal regulation in the Cowan–Farquhar scheme is unspecific, which prevents direct comparison of \( G_w \). But the response \( shape \) can be compared by setting \( \lambda ' = \partial E/\partial A \) at the initial \( G_w \) for profit maximization, and plotting the alternative \( G_w \) trajectory that maintains \( \lambda ' \) instead of profit maximization. When soil is wet, the \( G_w \) response to \( D_L \) can be quite similar (Fig. 9a, \( P_s = 0 \) curves; \( V_{max25} = 100 \mu \text{mol m}^{-2} \text{s}^{-1} \), \( T_A = 30 ^\circ \text{C} \)), which is consistent with support for a near-constant \( \partial E/\partial A \) over diurnal time frames of favourable soil moisture (e.g. Farquhar et al. 1980). It is also consistent with relatively low hydraulic cost under these conditions. However, as soil dries, the \( \lambda ' \) setting (reduced to match the lower initial \( G_w \)) predicts more severe closure with \( D_L \) (even to \( G_w \approx 0 \)) and more conservative water use versus profit maximization, which predicts \( \partial E/\partial A \) should rise with \( D_L \) (rather than stay constant).

Such a rise has been observed (Thomas et al. 1999; but see Buckley et al. 2016) and is also predicted if \( T_A \) increases with \( D_L \) beyond the photosynthetic optimum (simulations not shown). The response to \( P_s \) (constant \( D \)) is dramatically different in the two schemes: maintaining \( \lambda ' \) results in no stomatal closure and premature hydraulic failure (Fig. 9b, desiccation at the asterisk). Profit maximization predicts a strong closure response (and declining \( \partial E/\partial A \)) because of the rising cost of extracting water from drying soil. The reduction in \( \lambda ' \) with drier soil has been anticipated and observed, although its \( a \) \( priori \) specification remains very difficult (Cowan 1982; Makala et al. 1996; Thomas et al. 1999; Manzoni et al. 2011; Manzoni et al. 2013). The \( CO_2 \) response is also dramatically different: as \( C_w \) is increased from 15 Pa, maintaining \( \lambda ' \) initially results in stomatal opening, versus the expected closure response as predicted by profit maximization (Fig. 9c). This wrong-way response is consistent with a further need to adjust \( \lambda ' \) with \( C_w \) (Katul et al. 2010). Given their often divergent stomatal responses, it should be possible to deduce which optimization criterion is being followed (\( \lambda ' \) versus profit maximization) by analysing data sets of gas exchange and xylem pressure with strong variation in \( D \), \( P_s \) and \( C_w \) (Wolf et al. 2016a; Anderegg, W.R.L. unpublished).

Our optimization model awaits validation against specific data sets. But its qualitative consistency with observation and quantitative agreement with BBL is promising. It has theoretical and practical advantages over the Cowan–Farquhar scheme: it poses an optimization criterion consistent with competition for water, it is readily calculated from measurable traits and it automatically responds in realistic ways to the gamut of environmental cues. The profit maximization scheme can be integrated into existing stand- and ecosystem models, including the hydraulically sophisticated TReES (Mackay et al. 2015). The hope is that these larger-scale models will be significantly improved by a stomatal control routine that is based on physiologically relevant traits and processes, yet computationally tractable and lean in parameters.
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Figure 9. The response of leaf diffusive conductance ($G_w$) for profit maximization (black curves) versus the constrained optimization of Cowan & Farquhar (1977; grey curves) where marginal water use efficiency ($\lambda = \partial E/\partial A$) is constant at the initial value for profit maximization. (a) The response to leaf-air vapour pressure deficit ($D_v$) at three soil water potentials ($P_s$: 0, –0.75, –1.5 MPa). (b) Response to $P_s$: asterisk denotes point of hydraulic failure and canopy dessication. (c) Response to ambient CO$_2$ concentration ($C_a$).

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**SUPPORTING INFORMATION**

Additional Supporting Information may be found in the online version of this article at the publisher’s web-site:

Figure S1. Examples of how specific plant- and environmental parameters shifts the gain-cost (β–θ) optimization.

Figure S2. Example of how an exponential vulnerability curve shifts the gain-cost (β–θ) optimization in wet versus dry soil.